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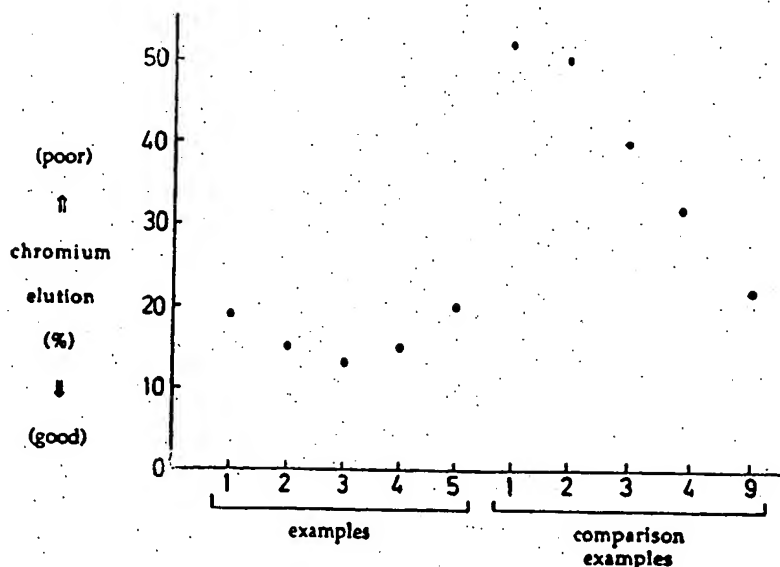
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INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

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(21) International Application Number: PCT/US90/05529 (22) International Filing Date: 27 September 1990 (27.09.90) (30) Priority data: 1 251165 27 September 1989 (27.09.89) JP (71) Applicant: HENKEL CORPORATION [US/US]; 300 Brookside Avenue, Ambler, PA 19002 (US). (72) Inventors: SAEKI, Kenshi ; 278-14, Hakuraku-cho, Kurashiki-shi, Okayama-ken 710 (JP). YOSHITAKE, Noriaki ; 3-8-710, Ohara, Hiratsuka-shi, Kanagawa-ken 254 (JP). (74) Agent: WISDOM, Norvell, E.; Henkel Corporation, 300 Brookside Avenue, Ambler, PA 19002 (US).		(81) Designated States: AT (European patent), BE (European patent), BR, CA, CH (European patent), DE (European patent)*, DK (European patent), ES (European patent), FR (European patent), GB (European patent), IT (European patent), LU (European patent), NL (European patent), SE (European patent). Published <i>With international search report.</i> <i>Before the expiration of the time limit for amending the claims and to be republished in the event of the receipt of amendments.</i> <i>Optionally</i> <i>0.1% Silica</i>

(54) Title: COMPOSITION AND PROCESS FOR CHROMATING GALVANIZED STEEL AND LIKE MATERIALS**(57) Abstract**

The resistance of chromated zinc surfaced steel objects, particularly plates and sheets, to extraction of hexavalent chromium by alkaline degreasing solutions used on the chromated objects, can be substantially increased by utilizing an aqueous acidic liquid chromating composition containing (A) about 9.6 to about 96 g/L, expressed as its stoichiometric equivalent as chromic acid, of total chromium; (B) about 2 to about 35 g/L of trivalent chromium ions; (C) about 1 to about 128 g/L of phosphate ions; and (D) about 0.3 to about 4 g/L of fluorozirconate ions, with the chromium ratio in the aqueous acidic liquid composition being about 0.41 to about 0.70, the chromic acid/fluorozirconate weight ratio being about 10 to about 40, and the $\text{PO}_4/\text{Cr}^{+3}$ ratio being greater than about 0.03, greater than or equal to about $\{(9.2)/(\text{the chromium ratio}) - 4.0\}$, and less than or equal to about $\{(9.2)(\text{the chromium ratio}) - 1.2\}$. The corrosion resistance of the coatings formed can be further improved if the chromating composition also contains about 0.1 to about 200 g/L of dispersed silica.

DESIGNATIONS OF "DE"

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COMPOSITION AND PROCESS FOR CHROMATING GALVANIZED STEEL
AND LIKE MATERIALS

BACKGROUND OF THE INVENTION

Field of the Invention

This invention relates to a process for chromating zinc surfaced steel objects to improve the resistance of the chromate coating formed to leaching by conventional aqueous based degreasing compositions, and to chromating solutions useful for such a process. The invention is applicable, for example, to all varieties of electroplated and/or dip coated forms of galvanized steel or zinc alloy coated steel, when the surface coating layer is metallic and is at least half zinc by weight. The film formed over the zinc surface has chromic acid or chromate as its principal component. This invention is particularly applicable to sheets and other flat zinc surfaced objects intended for later shaping into articles for ultimate use.

Statement of Related Art

It is known that the pre-painting and post-painting corrosion resistance of zinc surfaced steel objects may be improved by the formation of a chromate film on the objects, resulting from application to and drying on the sur-

faces of the objects of an acidic aqueous solution having chromic acid or chromate as its principal component. The chromium add-on in the chromate film formed on such a surface is generally from 5 to 200 milligrams per square meter ("mg/m²"), and the object is normally dried at temperatures of 60 to 150 degrees Centigrade. Steel sheet carrying the chromate film generated by such a treatment is then normally subjected to cutting and/or forming operations and subsequently painted after such steps as degreasing, rinsing, and the like.

With chromate films obtained by the methods now conventional in the art, part of the chromate film elutes into the degreasing solution during a conventional degreasing step, and this compromises the performance quality of the film. In addition, this eluting portion of the prior art chromate films is predominantly hexavalent chromium, and its contamination of the degreasing solution is disadvantageous because of the risk of environmental pollution.

One means for inhibiting this chromium elution is to increase the trivalent chromium content in the chromate coating solution. However, because a chromate coating solution can easily gel as the chromate coating process progresses, as a result of build up in the coating solution of eluted zinc and trivalent chromium produced by reduction, there are practical limitations on the trivalent chromium content that can be produced in the films, without causing instability of the chromate coating solutions.

Accordingly, the prior chromate coating solutions suffer from problems in terms of avoiding environmental pollution and/or coating solution stability.

DESCRIPTION OF THE INVENTION

Except in the claims and the operating examples, or where otherwise expressly indicated, all numbers in this description indicating amounts of material or conditions of reaction and/or use are to be understood as modified by the word "about" in describing the broadest scope of the invention. Practice within the exact numerical limits stated is

generally preferred.

Summary of the Invention

As a concrete means for solving the problems described above for the prior art, the present invention utilizes a chromate coating solution for zinc surfaced steel objects, particularly sheet. The chromate coating solution is an acidic aqueous solution and comprises, or preferably consists essentially of, water and:

(A) from 9.6 to 96 grams per liter ("g/L"), expressed as its stoichiometric equivalent as chromic acid, of total chromium;

(B) from 2 to 35 g/L of trivalent chromium ions;

(C) from 1 to 128 g/L of phosphate ions; and

(D) from 0.3 to 4 g/L of fluorozirconate ions.

In this specification of the composition, and in the additional specifications of the solution content given below, phosphoric acid itself and any anions produced by the partial ionization of phosphoric acid are considered as their stoichiometric equivalent as phosphate ions.

In addition to the compositional ranges given above, a chromate coating solution according to this invention conforms to the following conditions: (i) the ratio by weight of trivalent chromium ions to total chromium atoms in the solution, briefly denoted hereinafter as the "chromium ratio", is in the range from 0.41 to 0.70, or preferably in the range from 0.50 to 0.60; (ii) the ratio by weight of the total chromium content of the solution, expressed as its stoichiometric equivalent as chromic acid, to the fluorozirconate ion content, briefly denoted hereinafter as the "chromic acid/fluorozirconate ratio" or " $\text{CrO}_3/\text{ZrF}_6$ ", is from 10 to 40; and (iii) the ratio by weight of the phosphate ion content of the solution to the trivalent chromium ion content of the solution, briefly denoted hereinafter as the "phosphate/Cr(III) ratio" or " $\text{PO}_4^{3-}/\text{Cr}^{+3}$ ", is greater than 0.03, is greater than or equal to $((9.2)(\text{the chromium ratio}) - 4.0)$, and is less than or equal to $((9.2)(\text{the chromium ratio}) - 1.2)$.

Brief Description of the Drawings

Figure 1 is a graph showing chromate elution due to alkaline degreasing for the chromate coating solutions in Examples 1 to 5 of the present invention and Comparison Examples 1 to 9. Figure 2 is a graph which reports the corrosion resistance after alkaline degreasing for the same examples and comparison examples. Figure 3 shows by its shaded area the range of chromium ratios (on the horizontal axis) and phosphate/Cr(III) ratios (on the vertical axis) for which the solutions are stable against gelation, and shows the chromium ratios and the phosphate/Cr(III) ratios for the compositions of each of the examples and comparison examples.

Detailed Description of the Invention and of the Preferred Embodiments

The chromate coating solution composition as specified above inhibits chromium elution from the chromate film during subsequent degreasing of the chromate coated surface, while achieving adequate stability of the chromate coating solution against gelation.

Furthermore, the addition of silica at 0.1 to 200 g/L to a chromate coating solution within the compositional conditions noted above also results in the formation of a highly corrosion resistant chromate film on the surface of zinc surfaced steel objects.

The chromic acid in the chromate coating solution of the present invention is preferably obtained by the addition of chromic anhydride (i.e., CrO_3), while the trivalent chromium ion can be added directly or, preferably, may be obtained by converting part of the hexavalent chromium into trivalent chromium by the addition of a reductant such as tannic acid, starch, alcohol, hydrazine, sucrose, and the like. The phosphate ions may be added in the form of orthophosphoric acid, ammonium phosphate, and the like. The hexafluorozirconate IV ion (i.e., ZrF_6^{-2}) may be added as, e.g., $(\text{NH}_4)_2\text{ZrF}_6$, H_2ZrF_6 , and the like. The silica, if used, may be added directly in the form of finely divided

and suspended solid silica, available commercially or otherwise from known wet method or dry method processes for making finely divided silica.

5 The range for the chromium ratio in a chromating solution according to this invention is 0.41 to 0.70. The chromate film formed from solutions with values below 0.41 suffers from substantial chromium elution during water rinsing, hot-water rinsing, or alkaline degreasing. On the other hand, the film formed has a reduced corrosion
10 resistance when formed from solutions with chromium ratio values in excess of 0.70. At a chromium ratio within the range of 0.41 to 0.70, the chromate film formed on the surface of zinc surfaced steel sheet is uniform and is only very slightly susceptible to elution.

15 The phosphate ion and fluoro-zirconate ion are added in order to maintain the stability (by inhibiting gelation) of the chromate coating solution. The addition of phosphate ion at 1 to 128 g/L affords good stability without gelation, even for chromate coating solutions with a chromium
20 ratio of 0.70. The chromate coating solution will usually gel if it contains less than 1 g/L phosphate ion or if the phosphate/Cr(III) ratio is less than 0.03 or is less than ((9.2)(the chromium ratio) - 4.0). With phosphate concentrations in excess of 128 g/L, or with a phosphate/Cr(III)
25 ratio greater than ((9.2)(the chromium ratio) - 1.2), the chromate coating solution is very stable, but the chromate film obtained will contain large amounts of chromium phosphate and usually will not have a satisfactory corrosion resistance.

30 The stability of the chromate coating solution is improved by the addition of the fluoro-zirconate ion, and this component also advantageously etches the surface of the substrate to be chromated, while at the same time converting the metal ions dissolved during etching into a complex.
35 The result is that a firmly adherent chromate film can be obtained over long periods of use of the same chromating solution. There is little benefit from the fluoro-zirconate

ion at concentrations below 0.3 g/L. On the other hand, at concentrations in excess of 4 g/L, the surface of the substrate to be chromated is etched excessively and zinc is dissolved rapidly into the chromate coating solution. This shortens the useful life of the chromate coating solution. The chromic acid/fluorozirconate ion weight ratio in the chromate coating solution should fall within the range of 10 to 40. At below 10 or in excess of 40, neither a firmly adherent chromate film nor a highly stable chromate coating solution can usually be obtained.

The presence of silica at 0.1 to 200 g/L in the chromate coating solution of the present invention improves the corrosion resistance of the chromate film coated product. Almost no effect from silica addition is observed at below 0.1 g/L, while exceeding 200 g/L leads to an excessive film coating weight and a poorer adherence by the chromate film. Considering the properties of the chromate film, preferred silica additions will give a chromic acid/silica weight ratio of 10:1 to 1:2.

With regard to use of the chromate coating solution of the present invention, the preferred process steps are generally degreasing, then a water rinse, then chromate coating, and finally drying. Preferably there should be no rinsing between chromate coating and drying. The chromate coating solution is preferably used at room temperature to 50 degrees Centigrade, and may be applied by roll coating, spraying, immersion, or any other convenient method of making adequate contact between the surface to be chromated and the chromating solution. Immediately after application, excess coating may be removed by any convenient method, such as passing between rolls or the like. The chromate coating solution is preferably applied at a coating weight of 10 to 200 mg/m² and more preferably 15 to 100 mg/m², measured as chromium on the surface area coated. The chromate coating solution removed by, for example, a passage between rolls, may be collected and recycled to the solution coating stage.

Zinc passes into the chromate coating solution as use of a chromate coating solution according to this invention continues, and the properties of the chromate film obtained can be substantially affected by the balance between this zinc dissolution and the quantity of solution taken up by the zinc surfaced steel sheet. Some means known per se in the art for controlling the quantity of zinc in the coating solution should preferably be implemented during prolonged use of a process according to this invention. For example, withdrawing and discarding a constant volume fraction of the bath and replacing the withdrawn volume with freshly made solution during prolonged use, or passing the solution periodically through an ion exchanger to remove zinc, may be used.

The practice of the invention may be further appreciated by consideration of the following working examples and comparison examples.

Examples

The present invention is illustrated in the following Examples 1 to 5 and contrasted with Comparison Examples 1 to 9. The composition and stability of each chromate coating solution are reported in Table 1. These solutions were prepared by dissolving the amount of CrO_3 shown in the top line, together with the orthophosphoric acid and fluoro-zirconic acid required to give the amounts of phosphate ion and ZrF_6^{2-} shown respectively. The amount of Cr^{+3} shown was then generated in situ by reduction with methanol. Thus the concentration shown for CrO_3 in Table 1 is actually the stoichiometric equivalent as CrO_3 of the total chromium atom content of the solution as already discussed above.

A commercial oiled electrogalvanized (zinc quantity = 20 g/m^2) steel sheet was subjected to the following treatments in the order given: alkaline degreasing, water rinse, roll squeegee, roll coating of the chromate coating solution (at room temperature), and drying (maximum sheet temperature reached was 70 degrees Centigrade). The chromium add-on for the chromate films obtained was 60 mg/m^2 .

Table 1. Compositions of the Chromate Coating Solutions and Stability of the Chromate Coating Solutions

		Examples					Comparison Examples								
		1	2	3	4	5	1	2	3	4	5	6	7	8	9
chromate coating solutions		57.7	57.7	57.7	57.7	57.7	57.7	57.7	57.7	57.7	57.7	57.7	57.7	57.7	57.7
components	CrO ₃	12.3	15.0	18.0	21.0	15.0	-	3.0	6.0	9.0	15.0	18.0	21.0	24.0	24.0
	Cr ³⁺	0.41	0.50	0.60	0.70	0.50	0	0.10	0.20	0.30	0.50	0.60	0.70	0.80	0.80
	chromium ratio	6.5	12.5	37.8	76.7	12.5	-	6.5	6.5	6.5	6.5	12.5	37.8	76.7	131.5
	PO ₄ ³⁻ (H ₃ PO ₄)	2.3	2.3	2.3	2.3	2.3	-	2.3	2.3	2.3	2.3	2.3	2.3	2.3	2.3
	ZrF ₆ ²⁻ (H ₂ ZrF ₆)	25/1	25/1	25/1	25/1	25/1	-	25/1	25/1	25/1	25/1	25/1	25/1	25/1	25/1
(water)	CrO ₃ /ZrF ₆ ²⁻	0.53	0.83	2.10	3.65	0.83	-	2.17	1.08	0.72	0.43	0.69	1.80	3.20	5.48
	PO ₄ ³⁻ /Cr ³⁺	-	-	-	-	60	-	-	-	-	-	-	-	-	-
	SiO ₂ (silica sol)	+	+	+	+	+	+	+	+	+	x	x	x	x	+
chromate coating solution stability		+	+	+	+	+	+	+	+	+	x	x	x	x	+

The values in Figures 1 and 2 were determined by the following tests:

Chromium elution

The chromated samples were sprayed for 2 minutes at a spray pressure of 0.8 kilograms per square centimeter, using a 2 % by weight solution in water, at a temperature of 60 degrees Centigrade, of a conventional commercial medium alkaline degreaser based on sodium phosphate and sodium silicate. This chromating was followed by a water rinse and drying. The chromium adhering on the steel sheet was measured before and after this spraying treatment, and the % chromium elution is defined as $100(A_p - A_a)/A_p$, where A_p is the areal density of chromium add-on prior to the spraying treatment and A_a is the areal density of chromium after the spraying treatment.

Corrosion Resistance

After alkaline degreasing of the chromate film as described above, the samples were tested in a conventional salt spray test. The area of white rust development (as a percent of the total area) was examined and recorded after 100 and 200 hours of salt spray exposure.

Chromate Coating Solution Stability

After preparation of the chromate coating solution, its external appearance was inspected visually. The results are reported in Table 1: + = no abnormalities; x = gelation.

Benefits of the Invention

As has been explained above, a zinc surfaced steel product chromated according to this invention evidences a smaller amount of chromate elution than products treated with prior chromate coating solutions and thus substantially reduces environmental pollution. At the same time, a chromating solution composition according to this invention is relatively resistant to adverse effects from zinc dissolving into the solution during a fairly long time after being first made up, and can be continued in use much

longer when subjected to continuous treatment to counter the buildup of zinc in the solution. Thus the chromating solutions according to this invention have excellent long-term stability.

- 5 In addition, a chromate film can be formed which evidences an even better corrosion resistance when the acidic aqueous solution of the present invention contains dispersed silica at a concentration of 0.1 to 200 g/L.

What is claimed is:

CLAIMS

1. A process for protecting zinc surfaced steel objects against corrosion, said process comprising contacting the zinc surfaced steel objects for a sufficient time to form a chromate coating thereon, with an aqueous acidic liquid composition consisting essentially of water and:
- (A) from about 9.6 to about 96 g/L, expressed as its stoichiometric equivalent as chromic acid, of total chromium;
 - (B) from about 2 to about 35 g/L of trivalent chromium ions;
 - (C) from about 1 to about 128 g/L of phosphate ions; and
 - (D) from about 0.3 to about 4 g/L of fluorozirconate ions; and, optionally,
 - (E) from about 0.1 to about 200 g/L of dispersed silica, the chromium ratio in said aqueous acidic liquid composition being from about 0.41 to about 0.70, the chromic acid/fluorozirconate ratio in said aqueous acidic liquid composition being about 10 to about 40, and the phosphate/Cr(III) ratio in said aqueous acidic liquid composition being greater than about 0.03, greater than or equal to about $\{(9.2)(\text{the chromium ratio}) - 4.0\}$, and less than or equal to about $\{(9.2)(\text{the chromium ratio}) - 1.2\}$.
2. A process according to claim 1, wherein the chromium content in the chromate coating formed has an areal density between about 10 and about 200 mg/m².
3. A process according to claim 2, wherein the chromium content in the chromate coating formed has an areal density between about 15 and about 100 mg/m².
4. A process according to claim 3, wherein the chromium ratio in said aqueous acidic liquid composition is between about 0.50 and about 0.60.
5. A process according to claim 2, wherein the chromium ratio in said aqueous acidic liquid composition is between about 0.50 and about 0.60.

0.19/2
 $\frac{.1}{1000} = .0001 = .01\%$

6. A process according to claim 1, wherein the chromium ratio in said aqueous acidic liquid composition is between about 0.50 and about 0.60.
- 5 7. A process according to claim 6, wherein said aqueous acidic liquid composition contains at least about 0.1 g/l of dispersed silica.
8. A process according to claim 5, wherein said aqueous acidic liquid composition contains at least about 0.1 g/l of dispersed silica.
- 10 9. A process according to claim 4, wherein said aqueous acidic liquid composition contains at least about 0.1 g/l of dispersed silica.
10. A process according to claim 3, wherein said aqueous acidic liquid composition contains at least about 0.1 g/l of dispersed silica.
- 15 11. A process according to claim 2, wherein said aqueous acidic liquid composition contains at least about 0.1 g/l of dispersed silica.
12. A process according to claim 1, wherein said aqueous acidic liquid composition contains at least about 0.1 g/l of dispersed silica.
- 20 13. A process according to claim 12, comprising additional steps of drying the coated substrate after contacting it with said aqueous acidic liquid composition and subsequently degreasing the coated and dried substrate by contact with an aqueous alkaline liquid degreasing composition.
- 25 14. A process according to claim 7, comprising additional steps of drying the coated substrate after contacting it with said aqueous acidic liquid composition and subsequently degreasing the coated and dried substrate by contact with an aqueous alkaline liquid degreasing composition.
- 30

15. A process according to claim 3, comprising additional steps of drying the coated substrate after contacting it with said aqueous acidic liquid composition and subsequently degreasing the coated and dried substrate by contact with an aqueous alkaline liquid degreasing composition.

16. A process according to claim 2, comprising additional steps of drying the coated substrate after contacting it with said aqueous acidic liquid composition and subsequently degreasing the coated and dried substrate by contact with an aqueous alkaline liquid degreasing composition.

17. An aqueous acidic liquid composition of matter, consisting essentially of water and:

- (A) from about 9.6 to about 96 g/L, expressed as its stoichiometric equivalent as chromic acid, of total chromium;
- (B) from about 2 to about 35 g/L of trivalent chromium ions;
- (C) from about 1 to about 128 g/L of phosphate ions; and
- (D) from about 0.3 to about 4 g/L of fluorozirconate ions; and, optionally,
- (E) from about 0.1 to about 200 g/L of dispersed silica, the chromium ratio in said aqueous acidic liquid composition being from about 0.41 to about 0.70, the chromic acid/fluorozirconate ratio in said aqueous acidic liquid composition being about 10 to about 40, and the phosphate/Cr(III) ratio in said aqueous acidic liquid composition being greater than about 0.03, greater than or equal to about $\{(9.2)(\text{the chromium ratio}) - 4.0\}$, and less than or equal to about $\{(9.2)(\text{the chromium ratio}) - 1.2\}$.

18. A composition according to claim 17, comprising at least about 0.1 g/L of dispersed silica.

19. A composition according to claim 18, wherein the chromium ratio in said aqueous acidic liquid composition is between about 0.50 and about 0.60.

20. A composition according to claim 17, wherein the chromium ratio in said aqueous acidic liquid composition is between about 0.50 and about 0.60.

Figure 1.

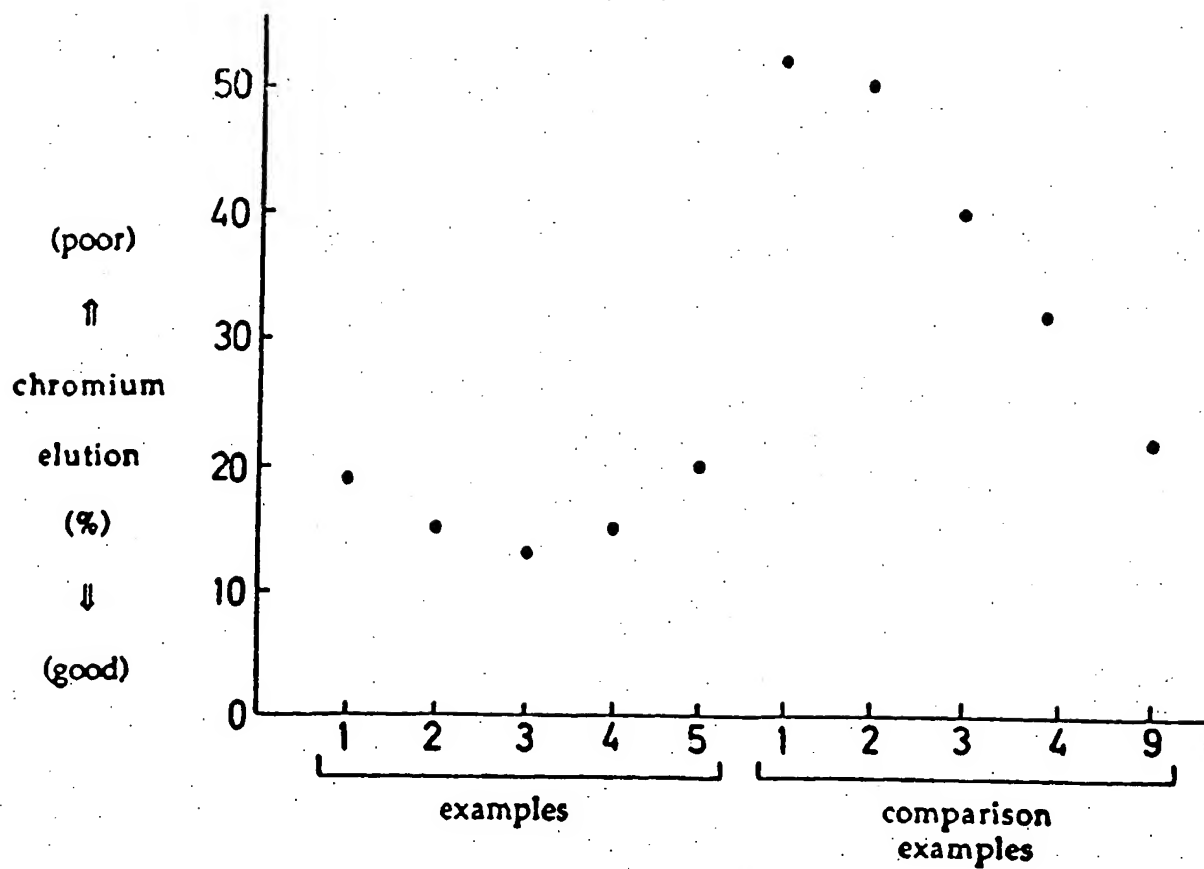
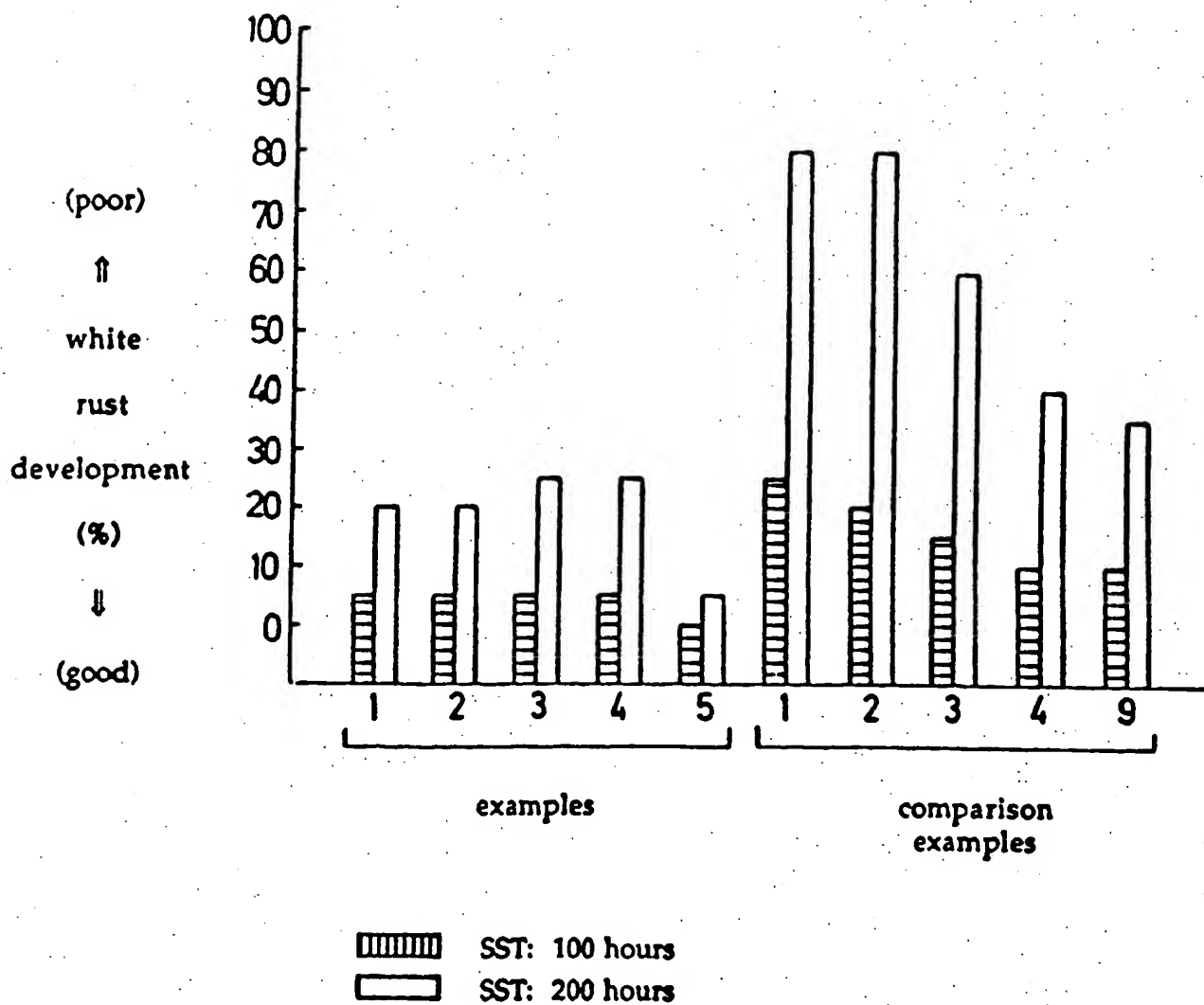
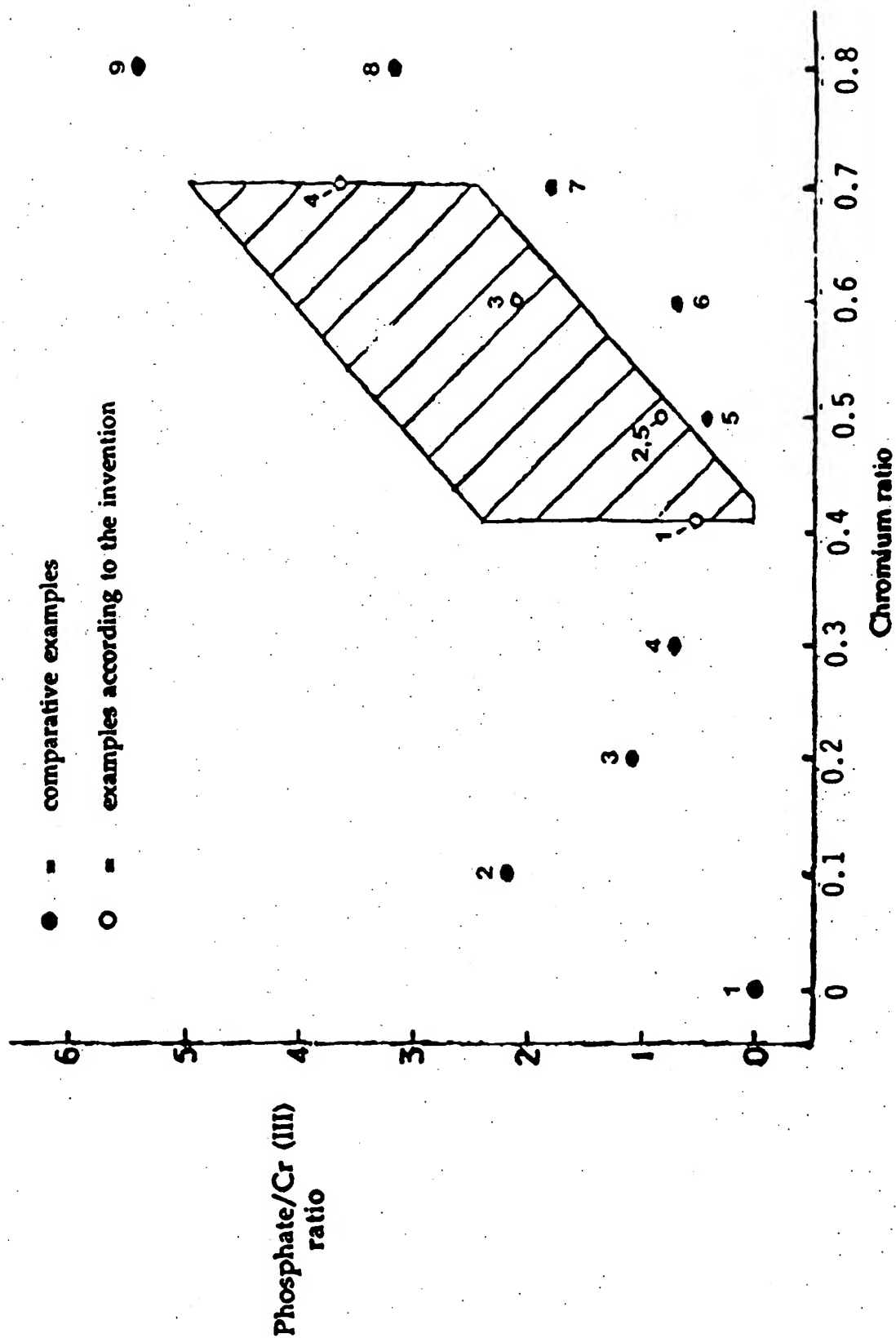


Figure 2.



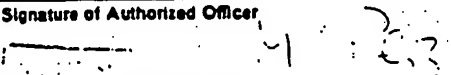
SUBSTITUTE SHEET

Figure 3.



INTERNATIONAL SEARCH REPORT

International Application No PCT/US 90/05529

I. CLASSIFICATION OF SUBJECT MATTER (If several classification symbols apply, indicate all) ⁶		
According to International Patent Classification (IPC) or to both National Classification and IPC		
IPC ⁵ : C 23 C 22/38		
II. FIELDS SEARCHED		
Minimum Documentation Searched ⁷		
Classification System	Classification Symbols	
IPC ⁵	C 23 C	
Documentation Searched other than Minimum Documentation to the Extent that such Documents are Included in the Fields Searched ⁸		
III. DOCUMENTS CONSIDERED TO BE RELEVANT ⁹		
Category ⁹	Citation of Document, ¹¹ with indication, where appropriate, of the relevant passages ¹²	Relevant to Claim No. ¹³
X	EP, A, 0214571 (NIHON PARKERIZING CO., LTD) 18 March 1987 see page 11, table 4; claims 1,2,3,6	1-3,10-12, 17,18
Y	--	13,15,16
Y	EP, A, 249206 (NIHON PARKERIZING CO., LTD) 16 December 1987 see example 1; pages 5,6; comparative example 1; pages 7,8	13,15,16
A	DE, A, 1521930 (PENNSALT CHEMICALS CORP.) 23 October 1969	
E	EP, A, 0391442 (HENKEL CORPORATION) 10 October 1990 see examples; page 6; claims 1,9	1,2,5,6,17, 20
	--	
	./.	
<p>¹⁰ Special categories of cited documents:</p> <p>"A" document defining the general state of the art which is not considered to be of particular relevance</p> <p>"E" earlier document but published on or after the international filing date</p> <p>"L" document which may throw doubt on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)</p> <p>"O" document referring to an oral disclosure, use, exhibition or other means</p> <p>"P" document published prior to the international filing date but later than the priority date claimed</p> <p>"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention</p> <p>"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step</p> <p>"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.</p> <p>"&" document member of the same patent family</p>		
IV. CERTIFICATION		
Date of the Actual Completion of the International Search		Date of Mailing of this International Search Report
28th January 1991		1. 12. 91
International Searching Authority		Signature of Authorized Officer
EUROPEAN PATENT OFFICE		

III. DOCUMENTS CONSIDERED TO BE RELEVANT (CONTINUED FROM THE SECOND SHEET)		
Category *	Citation of Document, " with indication, where appropriate, of the relevant passages	Relevant to Claim No.
P,X	EP, A, 0348890 (NKK CORPORATION) 3 January 1990 see page 3, line 55 - page 4, line 39; claims 1,2 -----	1-6,17,20

**ANNEX TO THE INTERNATIONAL SEARCH REPORT
ON INTERNATIONAL PATENT APPLICATION NO.**

US 9005529

SA 42069

This annex lists the patent family members relating to the patent documents cited in the above-mentioned international search report. The members are as contained in the European Patent Office EDP file on 19/02/91. The European Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
EP-A- 0214571	18-03-87	JP-A- 62056580	12-03-87
		CA-A- 1274156	18-09-90
		DE-A- 3629382	05-03-87
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EP-A- 0249206	16-12-87	JP-A, B, C 62294184	21-12-87
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